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Unprecedented Piezoresistance Coefficient in Strained Silicon Carbide

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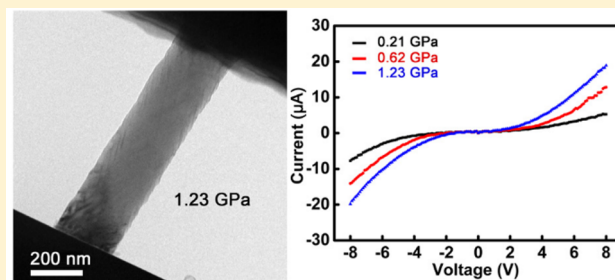
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Supporting Information

ABSTRACT: Reports reveal that the piezoresistance coefficients of silicon carbide (SiC) nanowires (NWs) are 2 to 4 times smaller than those of their corresponding bulk counterparts. It is a challenge to eliminate contamination in adhering NWs onto substrates. In this study, a new setup was developed, in which NWs were manipulated and fixed by a goat hair and conductive silver epoxy in air, respectively, in the absence of any depositions. The goat hair was not consumed during manipulation of the NWs. The process took advantage of the stiffness and tapered tip of the goat hair, which is unlike the loss issue of beam sources in depositions. With the new fixing method, in situ transmission electron microscopy (TEM) electromechanical coupling measurements were performed on pristine SiC NWs. The piezoresistance coefficient and carrier mobility of SiC NW are $-94.78 \times 10^{-11} \text{ Pa}^{-1}$ and $30.05 \text{ cm}^2 \text{ V}^{-1} \text{ s}^{-1}$, respectively, which are 82 and 527 times respectively greater than those of SiC NWs reported previously. We, for the first time, report that the piezoresistance coefficient of SiC NW is 17 times those of its bulk counterparts. These findings provide new insights to develop high performance SiC devices and to help avoid catastrophic failure when working in harsh environments.

KEYWORDS: Piezoresistance coefficient, strain, in situ TEM, electromechanical coupling, SiC



Strain engineering is considered as one of the most promising strategies for developing high performance devices at the nanoscale.^{1,2} It has been widely used to explore altering elementary properties such as band structure, to enhance the performance of a device.³ In fact, theory predicts that strain has a large effect on the band structure of nanowires (NWs), which in turn has an influence on their physical properties. Nanoscale devices aim to in part decrease the critical dimension to improve performance while reducing power consumption.⁴ Individual stressed semiconductor NWs have been demonstrated as an ideal material for exploring the strain-related electronic properties of devices.^{5,6} The piezoresistance coefficient of silicon (Si) NWs is 37.8 times that of

bulk Si.² This giant piezoresistance effect in strained NWs has significant implications in NW-based flexible electronics as well as in nanoelectromechanical system (NEMS). The piezoresistance effect converts elusive mechanical signals to easily accessible electrical signals at the nanoscale, enabling NWs to function as key building blocks of nanoscale devices.⁷ Nevertheless, Si has a low energy gap of 1.12 eV and is typically used at less than 200 °C because of the limitations of its physical and chemical properties.⁸

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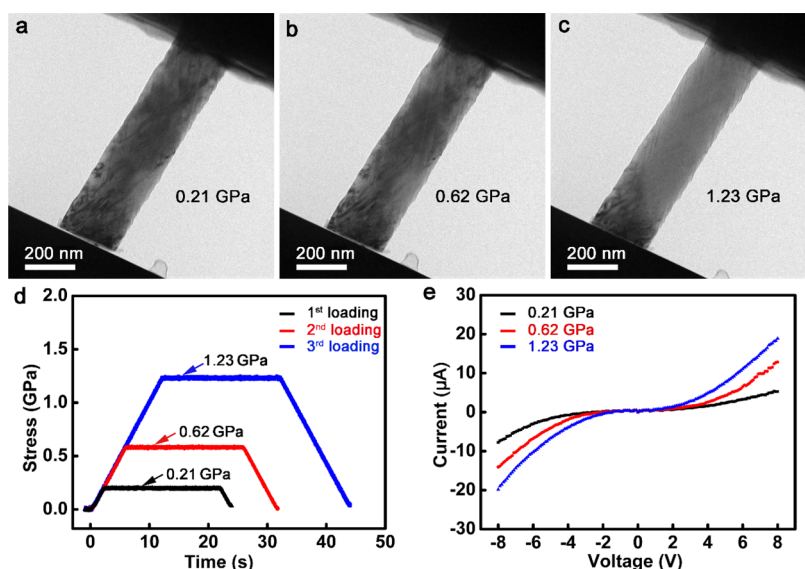


Figure 1. TEM images of an NW under axially compressive stress at (a) 0.21, (b) 0.62, and (c) 1.23 GPa; (d) stress and (e) current as a function of time and voltage, respectively, at three different axially compressive stresses.

Silicon carbide (SiC) has exceptional physical and mechanical properties, consisting of low density, high strength, high thermal conductivity, stability at high temperature, high resistance to shocks, low thermal expansion, high refractive index, good biocompatibility, wide bandgap, and chemical inertness.⁹ These properties make SiC suitable for use at high temperature,^{10,11} high power,¹² and high frequency as well as in harsh environments.^{13–15} SiC has become one of the most promising materials for power electronics, heterogeneous catalyst supports, wear resistance devices, and biomaterials.⁹ Fabrication methods originating from Si technology have been applied to SiC. As a result, SiC is widely used in electronic, optoelectronic, and electromechanical devices as well as substrates for growing high performance graphene.^{16–18} Double toughness is obtained in a SiC whisker-reinforced matrix through adding a small fraction of SiC NWs. SiC nanoresonators have higher frequencies than gallium arsenide (GaAs) and Si counterparts for a given dimension.¹² A higher piezoresistance coefficient is expected in SiC NWs as compared with bulk counterparts, on account of the increased surface-to-volume ratio. Nonetheless, the piezoresistance coefficients of SiC NWs^{19,20} are 2 to 4 times smaller than those of bulk counterparts. Thus, there are no reports on the higher piezoresistance coefficient in pristine SiC NWs as compared to bulk counterparts.⁸

There are three main effects on the measurement of physical properties of NWs, relating to size-strengthening, size-independence, and size-weakening. The tremendous difference among measurement results is attributed to the intrinsic limitations of various testing protocols.²¹ To evaluate the piezoresistance effect of SiC NWs, electromechanical coupling measurements are required, in which mechanical manipulations and electrical measurements should be conducted simultaneously. Conventionally, electrochemical coupling measurements are carried out by interfacing the NWs with lithographically fabricated electrodes.² This method inevitably has stability and reliability issues when subjected to mechanical forces. To solve this problem, electron beam deposition (EBD)^{20,22–24} and focused ion beam (FIB) deposition^{21,25} are employed to interface the NWs on samples. However, EBD

and FIB depositions will induce contamination and damage on the NWs. Electromechanical coupling measurements are sensitive to contamination and damage of the NWs, resulting in considerable discrepancy of measurements between deposited and pristine NWs. It is a challenge to eliminate the contamination and damage induced by such deposition methods.

In this study, a new setup was developed, where NWs were manipulated and fixed by a goat hair and conductive silver (Ag) epoxy, respectively. With this method, a new metrology was performed on pristine NWs by in situ transmission electron microscopy (TEM) electromechanical coupling measurements. An unprecedented piezoresistance effect was observed, and the fundamental mechanism was elucidated by ab initio simulations.

Results and Discussion. Figure S1 illustrates the scanning electron microscopy (SEM) and TEM images as well as electron energy dispersive spectroscopy (EDS) and Raman spectra of 3C-SiC NWs. Diameters of NWs vary from tens of to hundreds of nanometers, as illustrated in Figure S1(a). The selected area electron diffraction (SAED) pattern exhibits monocrystalline characteristics (Figure S1(b)), which is in good agreement with HRTEM images in Figures S1(c,d). The axial direction of the NW is along $\langle 111 \rangle$ orientation, as confirmed by the HRTEM image in Figure S1(c). Si and carbon elements are found in Figure S1(e), and there were no other elements observed. This reveals that the SiC NWs are pristine without doping elements. Raman spectra in Figure S1(f) with peaks at 796 and 970 cm^{-1} are consistent with those of single crystal 3C-SiC NWs.¹²

Figure S2(a) depicts the schematic diagram of the in situ TEM electromechanical measurement. The diameter and length of the NW in Figure S2(b) are 249 and 968 nm, respectively. An axially compressive force was applied by a flat tungsten (W) tip. During compression, a voltage was exerted to the NW, and the compressing current was simultaneously measured. In this process, in situ TEM measurements were performed to observe the variation of nanostructure under axially compressive stress. With this method, in situ TEM electromechanical measurement is conducted. The NW was

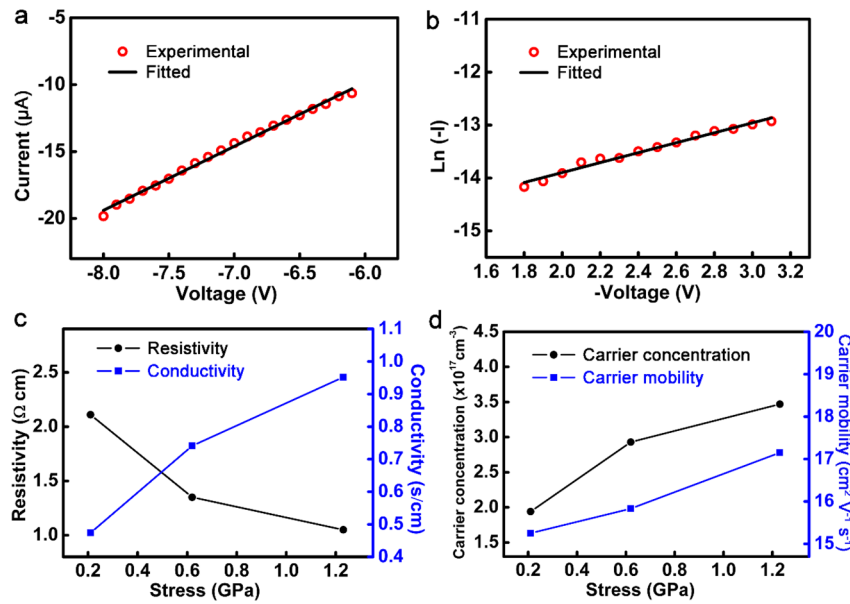


Figure 2. Experimental and fitted data of (a) current and (b) $\ln(-I)$ as a function of voltage at large and intermediate bias regimes, respectively, in Figure 3(e) at 1.23 GPa; (c) resistivity and conductivity and (d) carrier concentration and carrier mobility as a function of stress.

fixed by conductive Ag epoxy, absent of depositions, eliminating the contamination and damage induced by conventional depositions. Hence, an in situ TEM electro-mechanical measurement was developed to measure the piezoresistance effect of NWs.

Figure 1(a–c) shows the TEM images of an NW under axially compressive stress at 0.21, 0.62, and 1.23 GPa, respectively. Figure 1(d) shows the stress as a function of time at three different axially compressive stresses. In situ dynamic TEM electromechanical measurements of an NW at 10, 30, and 60 μN are played in Movies S1, S2, and S3, respectively. Current–voltage (I – V) curves in Figure 1(e) exhibit symmetrically nonlinear characteristics, indicating metal–semiconductor–metal (M–S–M) contact in W–SiC–Ag connections. The nonlinearity of I – V curves is because of the Schottky barrier between a metal and semiconductor.^{26–29} This is different from the ohmic contact induced by contaminations and damages of EBD^{20,22–24} and FIB^{21,25} depositions. In our work, a new setup was developed, in which NWs were manipulated and fixed by a goat hair and conductive Ag epoxy, respectively. Using the goat hair to manipulate NWs does not require depositions, and contaminations and damages are effectively eliminated. NWs were picked up by the goat hair tip in the developed setup. This function uses the stiffness and tapered tip of the goat hair, and the goat hair has no consumption during the operation on NWs, which is unlike the loss issue of beam sources taken place in depositions.

Figure 1(e) shows that the greater axially compressive stress leads to higher current and better electrical conductivity. According to the thermionic emission theory of the M–S–M structure, the I – V curve is linear at the large bias regime. Resistance of an NW is defined^{26,27}

$$R \approx \frac{dV}{dI} \quad (1)$$

where R is the resistance, and dV and dI are the differentials of the voltage and current, respectively. Figure 2(a) pictures the experimental and fitted data under a large bias regime of 1.23

GPa. The R of the NW in Figure 1(e) was calculated at 209.1 k Ω at 1.23 GPa. Resistivity, ρ , is presented

$$\rho = \frac{RA}{L} \quad (2)$$

where A and L are the area and length of an NW, respectively. According to eq 2, increasing the compressive stress in Figure 1(e), the area of the NW increases and the length decreases. If the resistance is invariable, resistivity increases, resulting, in a reverse manner, the decrease of resistance and increase of current. Conductivity, C , is calculated

$$C = \frac{1}{\rho} \quad (3)$$

ρ and C are 1.05 $\Omega \cdot \text{cm}$ and 0.95 s/cm , respectively. In Figures 1(e) and 2(b), a logarithmic plot of current I as a function of bias V gives approximately a straight line of slope, S ^{19,26,27}

$$S = \frac{q}{kT} - \frac{1}{E_0} \quad (4)$$

where q is the elemental charge, k is the Boltzmann constant, T is the temperature in Kelvin, and E_0 is a parameter that depends on the carrier density. E_0 is given²⁶

$$E_0 = E_{00} \coth\left(\frac{qE_{00}}{kT}\right) \quad (5)$$

where E_{00} is a parameter depending on the carrier density. E_{00} is obtained,^{19,26,27}

$$E_{00} = \frac{\hbar}{2} \left(\frac{N_d}{m^* \varepsilon} \right)^{1/2} = \frac{\hbar}{2} \left(\frac{N_d}{m_r m_r \varepsilon_r \varepsilon_0} \right)^{1/2} = 18.5 \cdot 10^{-15} \left(\frac{N_d}{m_r \varepsilon_r} \right)^{1/2} \text{ eV} \quad (6)$$

where \hbar is the Planck constant divided by 2π , N_d is the donor density between the metal and semiconductor interface, m^* ($=m_r m$) is the effective mass of an electron, ε ($=\varepsilon_r \varepsilon_0$) is the permittivity of an NW, m_r is the relative mass of an electron, m is the free-electron mass, ε_r is the relative permittivity of an

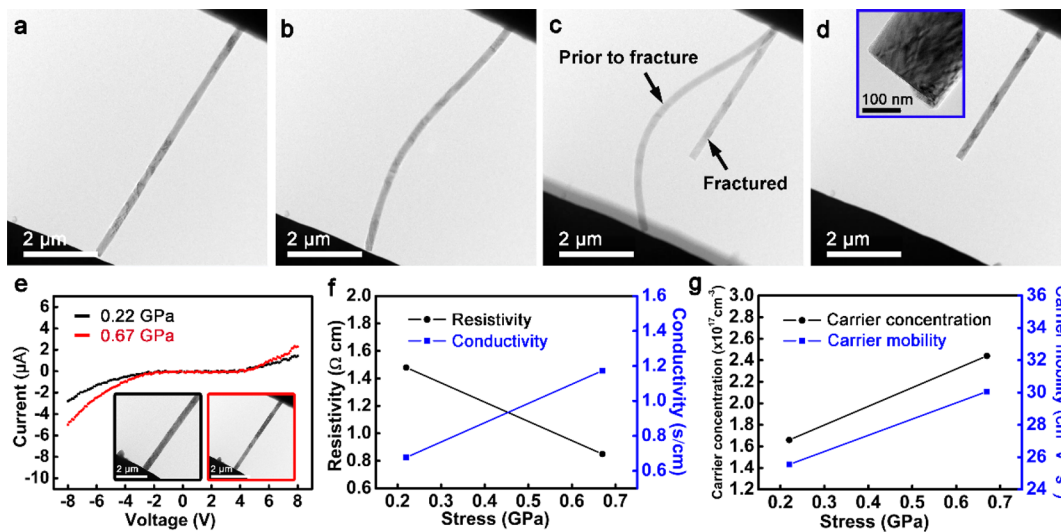


Figure 3. TEM images of an NW (a) prior to load, (b) under bending, (c) prior to and after fracture, as well as an (d) NW specimen with a fractured surface; (e) I – V curves at two axially compressive stresses; (f) resistivity and conductivity; and (g) carrier concentration and mobility as a function of stress. Inset in (d) shows the enlarged TEM image of the fractured surface. Insets in (e) show the TEM images of an NW under stresses at 0.22 and 0.67 GPa marked by black and red squares, respectively.

NW, and ϵ_0 is the permittivity of free space. Carrier mobility, μ , is calculated^{26,30}

$$\mu = \frac{1}{nq\rho} \quad (7)$$

where n is the carrier concentration. In the calculations, N_d is the same as n .²⁶ m_r and ϵ_r for 3C-SiC are 0.25³¹ and 9.72,³² respectively. The carrier concentration is $3.46 \times 10^{17} \text{ cm}^{-3}$ under compressive stress at 1.23 GPa. Resistivity and conductivity as a function of stress are illustrated in Figure 2(c). Carrier concentration and mobility under distinct compressive stress are depicted in Figure 2(d). Carrier concentration, mobility, and conductivity increases monotonically, whereas resistivity decreases with increasing compressive stress. To evaluate the piezoresistance effect of an NW, it is necessary to calculate the piezoresistance coefficient P_c .

$$P_c = \frac{\rho - \rho_0}{\sigma\rho_0} \quad (8)$$

where ρ_0 is the resistivity under zero stress, and ρ is the resistivity under stress σ . To contact well between the flat W tip and NW in Figure S2, an axially smaller compressive force of 10 μN is applied on the W tip. The measured σ_1 and ρ_1 are 0.21 GPa and 2.11 $\Omega\cdot\text{cm}$, respectively. P_c recasts as

$$P_c = \frac{\rho - \rho_1}{(\sigma - \sigma_1)\rho_1} \quad (9)$$

Piezoresistance coefficients $P_{c<111>}$ are -48.89×10^{-11} and $-87.81 \times 10^{-11} \text{ Pa}^{-1}$ under axially compressive stress at 1.23 and 0.62 GPa, respectively, corresponding to carrier mobilities of 17.13 and 15.93 $\text{cm}^2 \text{ V}^{-1} \text{ s}^{-1}$. The $P_{c<111>}$ of $-87.81 \times 10^{-11} \text{ Pa}^{-1}$ and carrier mobility of 15.93 $\text{cm}^2 \text{ V}^{-1} \text{ s}^{-1}$ are 76.35 and 279.48 times those of SiC NWs under tensile strain, in which the $P_{c<111>}$ and carrier mobility are $-1.15 \times 10^{-11} \text{ Pa}^{-1}$ and 0.057 $\text{cm}^2 \text{ V}^{-1} \text{ s}^{-1}$, respectively.¹⁹ The piezoresistance coefficient and carrier mobility measured in this study are unprecedented, compared with previous reports. A relationship is presented between gauge factor (GF) and piezoresistance coefficient¹⁹

$$\text{GF} = P_c Y \quad (10)$$

where Y is the Young's modulus. The Young's modulus of SiC NW along the $[111]$ orientation is 600 GPa.³³ The piezoresistance coefficient of bulk SiC varies from -2.12×10^{-11} to $-5.3 \times 10^{-11} \text{ Pa}^{-1}$.³⁴ In this work, the piezoresistance coefficient of NW is 16.56 times that of bulk SiC.

The NW devices are sometimes prepared and fabricated in vacuum. To investigate the piezoresistance effect of a clean surface, an NW was fractured under compression in the vacuum of the TEM, as shown in Figures 3(a–c). In Figure 3(c), there are two NWs present in an image. The two NWs are the same one prior to and after fracture because of the difference between the sample frequency of the camera in TEM and in situ TEM compression. In situ dynamic TEM compression of an NW is shown in Movies S4, S5, and S6 under compressive forces at 10, 30, and 32 μN , respectively. In the inset of Figure 3(d), the fracture is along the $\{111\}$ planes through cleavage. Accordingly, a clean surface of SiC NW is obtained in vacuum. I – V curves are shown in Figure 3(e) under axially compressive stress at 0.22 and 0.67 GPa. Nonlinear characteristics of I – V curves confirm the Schottky contact in W–SiC–Ag connections,^{26,27} which is in good agreement with those in Figure 1(e). Nevertheless, I – V curves in Figure 3(e) demonstrate an asymmetrical feature from forward to reverse bias regimes. This is distinct from that in Figure 1(e). It is because of that the NW in Figure 1(e) was exposed in air, resulting in impurities being absorbed and oxidation on the surface. However, the fractured surface in Figure 3(e) is fabricated in vacuum, absent of impurities and oxidation on the surface. Moreover, in Figure 3(e), one side is a clean surface fabricated in vacuum, and the other side absorbs impurities and oxidizes in air, leading to the asymmetrical characteristics of I – V curves. Conductivity, carrier concentration, and mobility increase with stress; this is associated with a concomitant decrease in resistivity as depicted in Figure 3(f,g). This is consistent with the results from Figures S2(c,d). The piezoresistance coefficient $P_{c<111>}$ and carrier mobility in Figure 3(e) are $-94.78 \times 10^{-11} \text{ Pa}^{-1}$ and 30.05 $\text{cm}^2 \text{ V}^{-1} \text{ s}^{-1}$ (Figure 3(g)), respectively, which are

82.42 and 527.25 times those of NWs under tensile strain reported in previous literature.¹⁹ The unprecedented piezoresistance coefficient of the NW is 17.88 times that of bulk SiC.³⁴ To confirm the unprecedented piezoresistance effect, photographs of a SiC NW device prior to and after pressing are illustrated in Figure S3, and the dynamic pressing process is displayed in Movie S7. Prior to pressing, the conductance of the SiC NW device is low compared with the imposed voltage, resulting an unlit light (Figure S3(a)). After impressing, the conductance increases and the resistance decreases, leading to light (Figure S3(b)). High temperature to some materials can be considered a harsh environment. Si devices typically do not function at temperatures exceeding 200 °C.⁸ The pressing was operated at 300 °C, which is out of the scope of working conditions for normal Si devices. This demonstrates that the unprecedented piezoresistance effect of the SiC NW device works well at high temperature.

To explore the mechanism of the unprecedented piezoresistance effect of SiC NW, ab initio simulations were carried out. A constructed crystalline model of SiC NW is shown in Figure 4(a). Yellow, blue, and white balls represent Si, carbon,

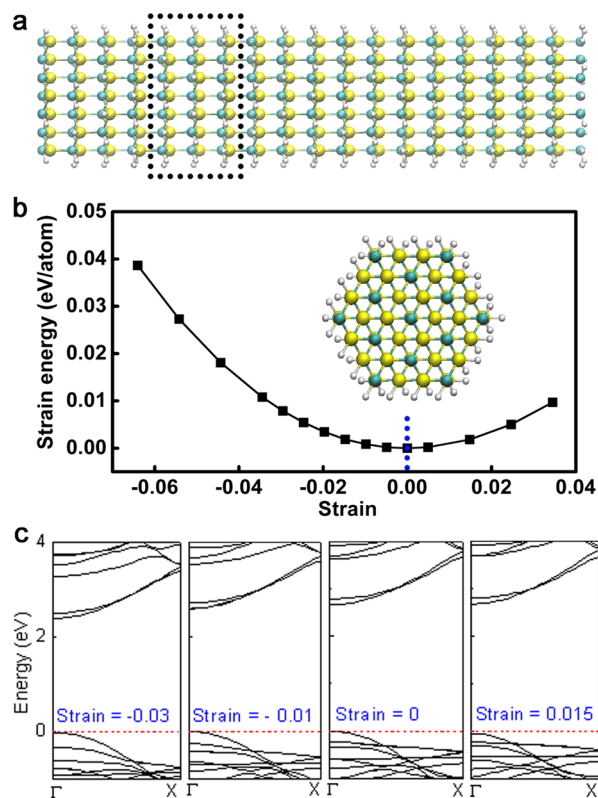


Figure 4. (a) Side view of the crystalline model of SiC NW used in ab initio simulations, (b) strain energy as a function of uniaxial strain, (c) band structure of the SiC NW at strains of -0.03 , -0.01 , 0 , and 0.015 . Inset in (b) shows the axial view of the NW in (a).

and hydrogen (H) atoms, respectively. The axial direction of the NW is along the $\langle 111 \rangle$ orientation, which agrees well with that in our experiment. A unit cell used in calculations is marked by a black dashed rectangle in Figure 4(a). The strain energy in Figure 4(b) reveals a parabolic shape, indicating that applied strain varying from -0.064 to 0.034 is in the elastic range. The representative electronic structure of the SiC NW is illustrated in Figure 4(c). A direct band gap of 2.67 eV is

observed between the top of the valence band and the doubly generated conduction band minimum at the Γ point. This is different from bulk SiC, which has an indirect band gap of 2.39 eV.³⁵ Values of SiC NWs with smaller diameters are above 3.31 eV³⁶ because of quantum confinement. Hence, the simulation results are in good agreement with previous results. In Figure 4(c), the lowest conduction band steadily approaches the Fermi level with increasing compressive strain, leading to a narrower band gap. The energy band gap monotonically decreases with decreasing strain over the entire region from tensile to compressive strain, as depicted in Figure 5(a). The smaller band gap induces higher probability of charge carrier transport, which is consistent with higher conductivity as shown in Figures 2(c) and 3(f) under axial compression. Variation of the effective mass of charge carriers with strain is shown in Figure 5(b). Both conduction band bottom and valence band top have an effective mass of $0.44m$. With applied axial strain, the effective mass reveals a negative correlation, on account of narrowing under compression and widening by tension of the band dispersion at the Γ point. Band edge shifts of the conduction band bottom and valence band top are illustrated in Figures 5(c,d), respectively. Most remarkable is that the slope, S , of the band edge shift of the conduction band bottom decreases dramatically, approaching to approximately zero under compressive strain (Figure 5(c)). The carrier mobility, μ , is estimated using the slope S ^{37,38}

$$\mu = \frac{2q\hbar^3 E}{3kT |m^*|^2 S^2} \quad (11)$$

where E is the elastic modulus. As a consequence, carrier mobility will significantly increase under compressive strain, which is in good agreement with unprecedented carrier mobility in Figures 2(d) and 3(g). The synergistic effect between reduced band gap and increased carrier mobility under compressive strain considerably increases the transport properties of SiC NWs. This contributes greatly to the unprecedented piezoresistance effect observed in our experiments.

In conclusion, a new setup was developed to eliminate the contamination and damage induced by conventional depositions to fix NWs. In the setup, NWs were moved and transferred by a goat hair and then fixed by a conductive Ag epoxy glue in air. With the new fixing method, in situ TEM electromechanical measurements were conducted on the NWs. Piezoresistance coefficient and carrier mobility of a SiC NW are $-87.81 \times 10^{-11} \text{ Pa}^{-1}$ and $15.93 \text{ cm}^2 \text{ V}^{-1} \text{ s}^{-1}$ under compressive stress respectively, which are 76.35 and 279.48 times those of SiC NWs previously reported. The unprecedented piezoresistance coefficient of SiC NW is 16.56 times that of bulk SiC. An NW was fractured under axial compression in the TEM, and then, in situ TEM electro-mechanical measurements were performed. The piezoresistance coefficient and carrier mobility of the fractured SiC NW are 82.42 and 527.25 times those reported previously. The unprecedented piezoresistance coefficient of SiC NW is 17.88 times that of its bulk counterparts. The outcomes found in this study pave a way to design and fabricate high performance semiconductor NW devices used in flexible electronics, NEMS, and nanoscale devices that could work at high temperature, high power, high frequency, and in harsh environments.

Experiments and Simulations. A TEM copper (Cu) grid with a diameter of 3 mm was used to manipulate SiC NWs.³⁸

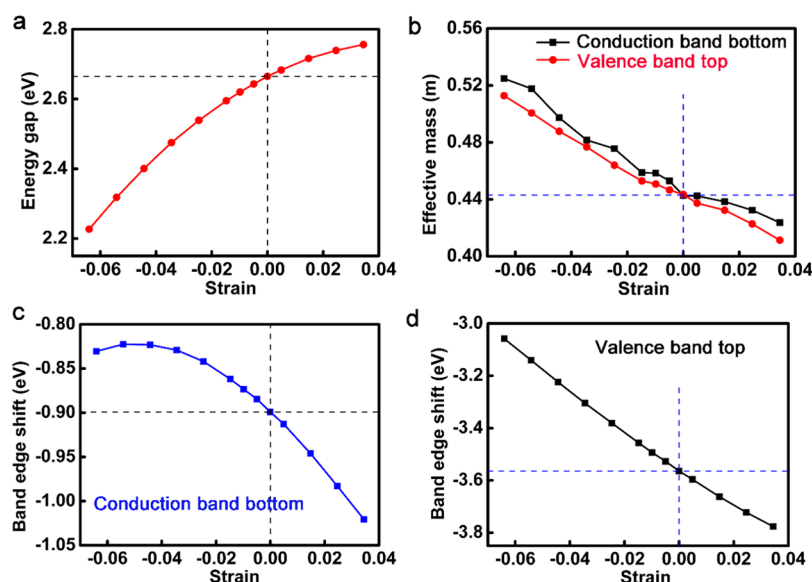


Figure 5. (a) Energy gap and (b) effective mass; band edge shift of (c) conduction band bottom and (d) valence band top as a function of strain.

A carbon film was covered on the Cu grid, which was removed by a fire ignited by a lighter. The Cu grid was then ultrasonically cleaned in acetone for 10 min. After the C film was removed, the uniform holes with a diameter of 100 μm on the Cu grid were exposed in air. NWs were put on the Cu grid, and they could be picked up using a goat hair through inserting the tapered tip into the hole and picking up the NW. This operation used the stiffness of the goat hair and attractive force between the goat hair and NW to overcome the force between the NW and Cu grid. Commercially available single crystal 3C-SiC NWs (Nanjing XFNANO Materials Tech Co., Ltd., China) were used as specimens for the in situ TEM electromechanical measurements. NWs were characterized and measured by SEM (Verios G4 UC, Thermo Scientific, USA), TEM (Talos F200X, Thermo Fisher Scientific, USA), and Raman spectra (Renishaw inVia Reflex, UK). They were ultrasonically dispersed in acetone solution for 3 min, and then, the solution was absorbed by a pipet. A drop of acetone containing the NWs was dripped on the Cu grid. After evaporation of acetone, the NWs were dispersed on the Cu grid. A goat hair was taken from a Chinese writing brush (Figure S4(a)). It was glued by conductive Ag epoxy (CircuitWorks Conductive Epoxy, CW2400, Chemtronics, USA) on a toothpick. The opposite sharp end of the toothpick was inserted on one side of a polyethylene foam cuboid, and another side was glued by double faced adhesive tape on a glass block. The glass block was put on a mechanical stage of another optical microscope (NMM-800RF, Ningbo Yongxin Optics Co., Ltd., China). The goat hair was operated in 3D spaces at millimeters and micrometers by the mechanical stage. To manipulate NWs, a new setup was developed (Figure S4(b)), in which the Cu grid was put on a mechanical stage of an optical microscope (Leica DM2500 M, Germany). The Cu grid on the mechanical stage was moved in three-dimensional (3D) space in millimeters and micrometers by coarse and fine focal adjustments. The goat hair had a tapered tip with diameters varied from several micrometers to hundreds of nanometers. An NW was picked up from the Cu grid by inserting the goat hair tip under the NW in a hole of the Cu grid (Figure S4(c)). After picking up, the Cu grid was replaced by a push-to-pull (PTP) device taken from an in situ TEM

nanomechanical system (PI 95 PicoIndenter, Hysitron, Minneapolis, USA). The NW was manipulated by the goat hair in the developed setup to put it on one side of the silicon-on-insulator (SOI) of the PTP device. It was fixed by conductive Ag epoxy onto the PTP (Figure S4(d)). To increase conductivity, a layer of conductive Ag paint was smeared on the surface of SOI. Then, the PTP device was mounted in the nanomechanical system. An in situ TEM system was inserted in a TEM (JEM-2100F, JEOL, Japan) to perform electromechanical coupling measurements. In situ TEM electromechanical measurements, mechanical force, and electrical signals were measured simultaneously. Meanwhile, the nanostructure of the NW was characterized and measured under strain. Mechanical force was applied by a load-controlled mode. The loading and unloading rates were 5 $\mu\text{N/s}$, and the holding time was 20 s. During holding, voltage was applied on the NW by the sweep mode. Voltages changed from -8 to 8 V, and current was measured at the same time. In each I - V curve, 160 points were measured, and each point lasted 50 ms.

Ab initio simulations were performed to investigate the electronic properties under strain for the unprecedented piezoresistance effect using the Vienna Ab initio Simulation Package (VASP) code.^{39,40} In the simulations, the generalized gradient approximation^{41,42} was employed in Perdew–Burke–Ernzerhof form for the exchange and correlation potential, which is together with the projector augmented wave (PAW) method.⁴³ The constructed crystalline model consisted of 116 atoms, and periodic conditions were applied to the axial direction. The surface layer of the model was passivated by H atoms to eliminate the effect of dangling bonds. An energy cutoff of 400 eV was chosen for the basis of the plane wave, and the model was fully relaxed when the forces on all atoms were less than 0.01 eV/Å. The fully relaxed SiC NW had a lattice constant of 7.644 Å in the axial direction, and the lateral size was 13.4 Å. The axial lattice constant was changed to simulate the strain under axial force.⁴⁴

■ ASSOCIATED CONTENT

Supporting Information

The Supporting Information is available free of charge on the ACS Publications website at DOI: 10.1021/acs.nanolett.9b02821.

Figure S1: SEM and TEM images as well as EDS and Raman spectra of SiC NWs; Figure S2: Schematic diagram of an in situ TEM electromechanical coupling measurement and TEM image of an NW prior to axial compression; Figure S3: Photographs of an SiC NW device prior to and after pressing working at 300 °C; Figure S4: Photographs of calligraphy written by a goat hair Chinese writing brush, a developed setup, optical image of a goat hair picking up an NW, and SEM image of an NW fixed by conductive Ag epoxy on a PTP device (PDF)

In situ dynamic TEM electromechanical measurements of an NW at 10 μ N (AVI)

In situ dynamic TEM electromechanical measurements of an NW at 30 μ N (AVI)

In situ dynamic TEM electromechanical measurements of an NW at 60 μ N (AVI)

In situ dynamic TEM compression of an NW under compressive force at 10 μ N (AVI)

In situ dynamic TEM compression of an NW under compressive force at 30 μ N (AVI)

In situ dynamic TEM compression of an NW under compressive force at 32 μ N (AVI)

Dynamic pressing process (AVI)

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Author Contributions

Z.Y.Z., N.J., and D.M.G. conceived the projects. Z.Y.Z. wrote the paper. J.F.C. designed and developed the operation method of NWs in air. J.F.C., D.D.L., D.L.Z., W.H., and H.H.L. performed the in situ TEM electromechanical measurements. C.T. conducted the ab initio simulations. Z.Y.Z., J.F.C., N.J., C.T., L.Z., C.Z., Y.L., and I.P.P. analyzed the mechanism of the unprecedented piezoresistance effect of SiC NWs under compressive strain. All authors discussed the results and commented on the manuscript.

Notes

The authors declare no competing financial interest.

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